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8217 DOI: 10.1021/acs.energyfuels.7b00877

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8534 DOI: 10.1021/acs.energyfuels.7b00895
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8580 DOI: 10.1021/acs.energyfuels.7b01329
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8594 DOI: 10.1021/acs.energyfuels.6b03393
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8631 DOI: 10.1021/acs.energyfuels.7b00709
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8643 DOI: 10.1021/acs.energyfuels.7b00723
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8648 DOI: 10.1021/acs.energyfuels.7b00883

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8655 DOI: 10.1021/acs.energyfuels.7b00922

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Effects of Different Additives on the Ignition and Combustion Characteristics of Micrometer-Sized Aluminum Powder in Steam
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Multi-environment Probability Density Function Modelling for Turbulent CH₄ Flames under Moderate or Intense Low-Oxygen Dilution Combustion Conditions with Recirculated Flue Gases
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Numerical Study of Flow and Heat Transfer of *n*-Decane with Pyrolysis and Pyrolytic Coking under Supercritical Pressures
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Analysis of the Formation and Interaction of Nitrogen Oxides in a Rapeseed Methyl Ester Nonpremixed Turbulent Flame
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Investigation of the NO Reduction Characteristics of Coal Char at Different Conversion Degrees under an NO Atmosphere
Zhuo-Zhi Wang, Jie Xu, Rui Sun,* Ya-Ying Zhao, Yu-Peng Li, and Tamer M. Ismail*

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Deposit Shedding in Biomass-Fired Boilers: Shear Adhesion Strength Measurements
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Direct Numerical Simulation Study on the Stabilization Mechanism of a Turbulent Lifted Pulverized Coal Jet Flame in a Heated Coflow
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Batteries and Energy Storage

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Facile and Efficient Synthesis of a Microsized SiO₂/C Core-Shell Composite as Anode Material for Lithium Ion Batteries
Junying Zhang, Xiaoming Zhang, Chunqian Zhang, Zhi Liu, Jun Zheng, Yuhua Zuo, Chunlai Xue, Chuanbo Li,* and Buwen Cheng

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Effects of Imidazolium-Based Ionic Liquids on the Rheological Behavior of Heavy Crude Oil under High-Pressure and High-Temperature Conditions
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Flame Images for Oxygen Content Prediction of Combustion Systems Using DBN
Yi Liu, Yu Fan, and Junhui Chen*

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Contactless Asphaltene Detection Using an Active Planar Microwave Resonator Sensor
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A MIL-101(Cr) and Graphene Oxide Composite for Methane-Rich Stream Treatment
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Experimental Study on the Removal of VOCs and PAHs by Zeolites and Surfactant-Modified Zeolites
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Comprehensive Analysis of the Coal Particle in Molten Blast Furnace Slag To Recover Waste Heat
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Correction to Impact of Pre-equilibration on the Assessment Methodology of Interfacial Tension Measured between Aqueous and Heavy Oil Phases

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Correction to Detection and Impact of Carboxylic Acids at the Crude Oil–Water Interface

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Correction to Interfacial Films Adsorbed from Bitumen in Toluene Solution at a Toluene–Water Interface: A Langmuir and Langmuir–Blodgett Film Approach

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Review on Surfactant Flooding: Phase Behavior, Retention, IFT, and Field Applications

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ABSTRACT: Surfactant flooding is an important technique used in enhanced oil recovery to reduce the amount of oil in pore space of matrix rock. Surfactants are injected to mobilize residual oil by lowering the interfacial tension between oil and water and/or by the wettability alteration from oil-wet to water-wet. A large number of cationic, anionic, non-ionic, and amphoteric surfactants have been investigated on a laboratory scale under different conditions of temperature and salinity. Selection of the appropriate surfactant is a challenging task, and surfactants have to be evaluated by a series of screening techniques. Different types of surfactants along with their limitations are reviewed with particular emphasis on the phase behavior, adsorption, interfacial tension, and structure–property relationship. Factors affecting the phase behavior, interfacial tension, and wettability alteration are also discussed. Field applications of surfactants for chemical enhanced oil recovery in carbonate and sandstone reservoirs are also reviewed. Finally, some recent trends and future challenges in surfactant enhanced oil recovery are outlined. Field studies show that most of the surfactant flooding has been conducted in low-temperature and low-salinity sandstone reservoirs. However, high-temperature and high-salinity carbonate reservoirs are still challenging for implementation of surfactant flooding.

1. INTRODUCTION

Oil has been the most important and significant source of energy so far, and it will contribute significantly in meeting the future energy demand as well.¹ Thus, it is necessary to enhance the current production level in the next few decades, which can be achieved by either discovering new fields or increasing the production from existing oil fields. Only about one-third of the oil present in a reservoir can be recovered using primary and secondary recovery techniques.^{2–5} Oil is initially recovered from a reservoir using the inherent pressure of the reservoir (primary recovery). After the dissipation of the initial pressure, oil is recovered by applying external pressure using seawater injection into the reservoir (secondary recovery). Enhanced oil recovery (EOR) or tertiary recovery techniques are used to recover the remaining oil which cannot be recovered using water flooding.⁶ Although chemical EOR (cEOR) is one of the most promising methods available to recover residual and remaining oil, it was not very commonly employed in the past due to low oil prices and the high cost of chemicals. However, continuous rise in oil prices and the growing demand for oil have encouraged researchers to determine economical and low-cost cEOR technology to recover the maximum amount of the remaining oil.

In cEOR, a range of chemicals such as surfactants, polymers, and/or alkalis are used to increase the microscopic efficiency (displacement efficiency) and the macroscopic efficiency (volumetric sweep efficiency).^{7–16} Macroscopic efficiency is related to the effectiveness of the displacing fluid in sweeping out the reservoir volume both areally and vertically as well as moving the oil toward the production well.¹⁷ Macroscopic efficiency can be increased using mobility control methods. Polymers are used to increase the viscosity of the displacing

fluid (water), which improves the oil/water mobility ratio.^{18–21} On the other hand, microscopic efficiency is related to the displacement of oil at the pore scale. It is not possible to displace all the oil that comes into contact with water during water flooding, due to trapping of oil by capillary forces. The relationship between the capillary forces and the viscous forces results in a dimensionless capillary number ($\mu v / \gamma \cos \theta$), where μ is the viscosity of the aqueous phase, v is the velocity, γ is the interfacial tension between oil and water, and θ is the contact angle.^{22,23} Microscopic efficiency can be improved by decreasing the capillary forces and the oil/water interfacial tension. Capillary number is closely related to oil recovery and residual oil saturation (oil saturation is the volume fraction of oil within the pore volume) and is in the range of 10^{-7} to 10^{-6} for typical brine flooding. Increasing the capillary number to between 10^{-4} and 10^{-3} reduces the oil saturation to 90%,⁶ and residual oil saturation approaches zero if the capillary number reaches 10^{-2} .²⁴ In order to reach this value, the interfacial tension (IFT) should be decreased from an initial value of 20–30 mN/m to values in the range of 10^{-2} to 10^{-3} ,²⁵ which is achieved through the use of surfactants during flooding with brine.^{26–28} Surfactants also influence the amount of residual oil recovered via other mechanisms, including microemulsification of trapped residual oil, changing the wettability of rock, and improving the interfacial rheological properties.^{29–30} Here wettability is defined as "the tendency of one fluid to adhere to a solid surface in the presence of another immiscible fluid".

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